SPECIFICATION

TO ALL WHOM IT MAY CONCERN:

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MULTI-WAVELENGTH LIGHT AMPLIFIER

of which the following is a specification : -

TITLE OF THE INVENTION

MULTI-WAVELENGTH LIGHT AMPLIFIER

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BACKGROUND OF THE INVENTION

1. Field of the Invention

The present invention generally relates to a light amplifier for a wavelength division multiplexed (WDM) optical transmission system, and more particularly to a light amplifier having a two-stage configuration which eliminates a wavelength-dependence of the gain of the light amplifier.

Recently, an optical communications network has increasingly been used in practice. Nowadays, it is required that the optical communications network cope with multi-media networking. A WDM system is more attractive, particularly in terms of an increase in the transmission capacity. In order to realize the WDM system, it is necessary to use a multi-wavelength light amplifier capable of amplifying a wavelength division multiplexed signal. It is required that such a multi-wavelength light amplifier does not have wavelength-dependence of the gain, which is further required not to be changed due to a variation in the power of the input light.

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~~A light amplifier is known which has an optical fiber doped with a rare-earth element and directly amplifies the input light. There has been some activity in the development of a multi-wavelength light amplifier which amplifiers a wavelength division multiplexed light signal including signal components having different wavelengths (channels).~~

However, normally, the rare-earth-element doped fiber amplifier has a very narrow range in which the gain thereof does not have the wavelength-dependence. In this regard, nowadays, there is no available light amplifier which can practically be used for the WDM system. That is, there is n

available light amplifi r which do s not hav wavelength-dependence of the gain, which is not changed due to a variati n in the power f the input light. Particularly, the wavelength-dependence of the gain, which takes place when the input power changes, deteriorates the signal-to-noise ratio with respect to a particular signal. This prevents the multi-wavelength light amplifier from being used in practice.

SUMMARY OF THE INVENTION

It is a general object of the present invention to provide a multi-wavelength light amplifier in which the above disadvantages are eliminated.

A more specific object of the present invention is to provide a multi-wavelength light amplifier which does not have wavelength-dependence of the gain, which is not changed due to a variation in the power of the input light.

The above objects of the present invention are achieved by a multi-wavelength light amplifier comprising: a first-stage light amplifier which has a first light amplifying optical fiber amplifying a light input; a second-stage light amplifier which has a second light amplifying optical fiber amplifying a first light output from the first-stage light amplifier; and an optical system which maintains a second light output of the second-stage light amplifier at a constant power level. The first-stage and second-stage light amplifiers have different gain vs wavelength characteristics so that the multi-wavelength light amplifier has no wavelength-dependence of a gain.

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The above multi-wavelength light amplifier may b configured as f llows. Th first-stage light amplifier comprises a first pump source which pumps

the first light amplifying optical fiber s as to have a first gain vs wavelength characteristic in which as a wavelength of light to be amplified becomes shorter, a gain of the first-stage light amplifier becomes higher. The second-stage light amplifier comprises a second pump source which pumps the second light amplifying optical fiber so as to have a second gain vs wavelength characteristic in which as a wavelength of light to be amplified becomes longer, a gain of the first-stage light amplifier becomes higher.

The above multi-wavelength light amplifier may be configured as follows. The first-stage light amplifier comprises a first pump source which pumps the first light amplifying optical fiber so as to have a first gain vs wavelength characteristic having a first linear gain slope. The second-stage light amplifier comprises a second pump source which pumps the second light amplifying optical fiber so as to have a second gain vs wavelength characteristic having a second linear gain slope. A combination of the first and second linear gain slopes results in a flat gain vs wavelength characteristic of the multi-wavelength light amplifier.

The above multi-wavelength light amplifier may further comprise an optical filter which emphasizes the gain vs wavelength characteristic of the first-stage light amplifier.

The above multi-wavelength light amplifier may further comprise an optical filter which compensates for a difference between the gain vs wavelength characteristics of the first-stage light amplifier and the second-stage light amplifier.

The above multi-wavelength light amplifier may be configured as follows. The optical filter is provided s as to follow the first-stage light amplifier. The first-stage light amplifier c mprises a first pump source which pumps the first light

amplifying ptical fiber s as t have a first gain vs wavelength characteristic having a first linear gain slope. The second-stage light amplifier comprises a second pump source which pumps the second light amplifying optical fiber so as to have a second gain vs wavelength characteristic having a second linear gain slope. The optical filter emphasizes the first linear gain slope to provide an emphasized first linear gain slope. A combination of the emphasized first linear slope and the second linear gain slope results in a flat gain vs wavelength characteristic of the multi-wavelength light amplifier.

The above multi-wavelength light amplifier may be configured as follows. The optical filter is provided so as to follow the first-stage light amplifier. The first-stage light amplifier comprises a first pump source which pumps the first light amplifying optical fiber so as to have a first gain vs wavelength characteristic having a first linear gain slope. The second-stage light amplifier comprises a second pump source which pumps the second light amplifying optical fiber so as to have a second gain vs wavelength characteristic having a second linear gain slope. The optical filter compensates for the difference between the first and second linear gain slopes so that a flat gain vs wavelength characteristic of the multi-wavelength light amplifier can be obtained.

The above multi-wavelength light amplifier may be configured as follows. The first-stage light amplifier has a first AGC (automatic gain control) system so that a ratio of the input light and the first light output is constant. The second-stage light amplifier has a second AGC system so that a ratio of the first light output and the second light output is c nstant.

The above multi-wavelength light amplifier

may be c nfigured as follows. The first-stage light amplifier has an AGC (automatic gain c ntr l) system so that a rati of the input light and the first light output is constant. The second-stage light amplifier has an automatic power control (APC) system so that the second light amplifying optical fiber is pumped at a predetermined constant power level.

The above multi-wavelength light amplifier may be configured as follows. The first-stage light amplifier has an AGC (automatic gain control) system so that a ratio of the input light and the first light output is constant. The second-stage light amplifier has an automatic level control (ALC) system so that the second light output is maintained at a predetermined constant power level.

The above multi-wavelength light amplifier may be configured as follows. The first AGC system comprises first means for detecting a first level of the light input and a second level of the first light output and pumping the first light amplifying optical fiber so that a ratio of the first and second levels is maintained at a first predetermined constant value. The second AGC system comprises second means for detecting a third level of the first light output and a fourth level of the second light output and pumping the second light amplifying optical fiber so that a ratio of the third and fourth levels is maintained at a second predetermined constant value.

The above multi-wavelength light amplifier may be configured as follows. The first-stage light amplifier has a first AGC (automatic gain control) system which detects a first amplified spontaneous emission of the first light amplifying optical fiber and pumps the first light amplifying optical fiber so that the first amplified spontaneous emissi n is maintain d at a first predetermined constant level. The second-stage light amplifier has a second AGC

system which detects a sec nd amplified sp ntaneous emission f the second light amplifying optical fiber and pumps the second light amplifying optical fiber so that the second amplified spontaneous emission is maintained at a second predetermined constant level.

The above multi-wavelength light amplifier may be configured as follows. The first-stage light amplifier has a first AGC (automatic gain control) system which detects a first pump light propagated through the first light amplifying optical fiber and pumps the first light amplifying optical fiber so that the first pump light is maintained at a first predetermined constant level. The second-stage light amplifier has a second AGC system which detects a second pump light propagated through the second light amplifying optical fiber and pumps the second light amplifying optical fiber so that the second pump light is maintained at a second predetermined constant level.

The above multi-wavelength light amplifier may be configured as follows. The first-stage light amplifier comprises a first pump source which pumps the first light amplifying optical fiber through a first coupler so as to have a first gain vs wavelength characteristic in which as a wavelength of light to be amplified becomes shorter, a gain of the first-stage light amplifier becomes higher. The second-stage light amplifier comprises a second pump source which pumps the second light amplifying optical fiber through a second coupler so as to have a second gain vs wavelength characteristic in which as a wavelength of light to be amplified becomes longer, a gain of the first-stage light amplifier becomes higher. At least one of the first and second couplers has a characteristic which emphasizes ne of the gain vs wavelength characteristics of the first-stage and second-stage light amplifi rs.

The ab ve multi-wav l ngth light amplifier may be c nfigured as f llows. The optical system which maintains the second light output of the second-stage light amplifier at a constant power level comprises a variable attenuator which is provided between the first-stage light amplifier and the second-stage light amplifier and attenuates the first output signal on the basis of the power level of the second light output.

The above multi-wavelength light amplifier may be configured as follows. The optical system which maintains the second light output of the second-stage light amplifier at a constant power level comprises a variable attenuator which is provided so as to follow the second-stage light amplifier and attenuates the second output signal on the basis of the power level of an attenuated second light output from the variable attenuator.

The above multi-wavelength light amplifier may be configured as follows. The optical system which maintains the second light output of the second-stage light amplifier at a constant power level comprises a variable attenuator which is provided between the first-stage light amplifier and the second-stage light amplifier and attenuates the first output signal on the basis of the power level of an attenuated first light output from the variable attenuator.

The above multi-wavelength light amplifier may further comprise a rejection filter which is provided between the first-stage light amplifier and the second-stage light amplifier and prevents a pump light which pumps the first light amplifying optical fiber from being transmitted to the second-stage light amplifier.

BRIEF DESCRIPTION OF THE DRAWINGS

Other bj cts, features and advantages of the present inv nti n will become m r apparent fr m the following detailed description when read in conjunction with the accompanying drawings, in which:

Fig. 1 is a block diagram of a multi-wavelength light amplifier according to a first embodiment of the present invention;

Fig. 2 is a diagram showing a principle of a multi-wavelength light amplifier according to a second embodiment of the present invention;

Fig. 3 is a block diagram of a multi-wavelength light amplifier according to a third embodiment of the present invention;

Fig. 4 is a diagram showing a principle of the multi-wavelength light amplifier according to the third embodiment of the present invention;

Fig. 5 is a block diagram of a multi-wavelength light amplifier according to a fourth embodiment of the present invention;

Fig. 6 is a diagram showing a principle of the multi-wavelength light amplifier according to the fourth embodiment of the present invention;

Figs. 7A and 7B are diagrams showing a principle of a multi-wavelength light amplifier according to a fifth embodiment of the present invention;

Fig. 8 is a block diagram of a multi-wavelength light amplifier according to a seventh embodiment of the present invention;

Fig. 9 is a block diagram of a multi-wavelength light amplifier according to an eighth embodiment of the present invention;

Fig. 10 is a block diagram of a multi-wavelength light amplifier according to a ninth embodiment of the pr sent invention;

Fig. 11 is a block diagram of a multi-wavelength light amplifier according to a tenth

embodiment f the present inventi n;

Fig. 12 is a block diagram f a multi-wavelength light amplifier acc rding to an eleventh embodiment of the present invention;

Fig. 13 is a block diagram of a multi-wavelength light amplifier according to a twelfth embodiment of the present invention;

Fig. 14 is a block diagram of a multi-wavelength light amplifier according to a thirteenth embodiment of the present invention; and

Fig. 15 is a block diagram of a multi-wavelength light amplifier according to a fourteenth embodiment of the present invention.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

Fig. 1 is a block diagram of a multi-wavelength light amplifier according to a first embodiment of the present invention. The amplifier shown in Fig. 1 includes a first-stage (front-stage) light amplifier 1 and a second-stage (rear-stage) light amplifier 2. A variable attenuator (ATT) 11 is provided between the first and second amplifiers 1 and 2. The variable attenuator 11 is controlled by an automatic level control (ALC) circuit 14, which is controlled by a photodetector 13 such as a photodiode. The photodiode 13 receives split light from a beam splitting coupler 12, which follows the second-stage amplifier 2. An optical system having a feedback loop is formed by the light splitting coupler 12, the photodiode 13, the ALC circuit 14 and the variable attenuator 11.

The first-stage amplifier 1 includes a first-stage light input monitor made up of a beam splitting coupler 3_1 and a photodiode 4_1, and a first-stage light output monitor made up of a beam splitting c upler 3_2 and a phot di d 4_2. Further, the first-stage amplifier 1 includes a light amplifying optical

fiber 7 such as a rare-earth-element d ped optical fiber and an exciting-light source (hereinafter referred to as a pump source: PS) 9_1, which is controlled by an automatic gain control (AGC) circuit 6_1 provided in the first-stage amplifier 1. An AGC system including the AGC circuit 6_1 and the above input and output monitors performs an AGC control of the pump source 9_1 so that the ratio of the light input power level detected by the light input monitor and the light output power level detected by the light output monitor can be maintained at a constant value. The above ratio corresponds to the gain of the first-stage amplifier 1.

The second-stage amplifier 2 includes a second-stage light input monitor made up of a beam splitting coupler 3_3 and a photodiode 4_3, and a second-stage light output monitor made up of a beam splitting coupler 3_4 and a photodiode 4_4. Further, the second-stage amplifier 2 includes a light amplifying optical fiber 8 such as rare-earth-element doped optical fiber, and a pump source 9_2, which is controlled by an AGC circuit 6_2 provided in the second-stage amplifier 2. An AGC system including the AGC circuit 6_2 and the above input and output monitors performs a AGC operation of the pump source 9_2 so that the ratio of the light input power level detected by the light input monitor and the light output power level detected by the light output monitor can be maintained at a constant value.

The combination of the first-stage amplifier 1 and the second-stage amplifier 2 functions to cancel the difference between the gain of the amplifier 1 and the gain of the amplifier 2 in each of the wavelengths of the multiplexed signal. That is, the amplifiers 1 and 2 have different gain vs. wav length characteristics (which may be simply referred to as gain characteristics), which can be compensated by the

combination of the amplifiers 1 and 2. As a result, the ntir multi-wavelength light amplifier has a flat gain vs wavelength characteristic.

It will now be assumed that $G_{0,1}$ denotes an AGC control setting level which causes the amplifier 1 to have a flat gain vs wavelength characteristic in which the output spectra at the respective wavelengths of the multiplexed signal have a constant peak value. Similarly, $G_{0,2}$ is denoted as an AGC control setting level which causes the amplifier 2 to have a flat gain vs wavelength characteristic in which the output spectra at the respective wavelengths of the multiplexed signal have a constant peak value. In order to achieve the above cancellation, the practical AGC control setting levels G_1 and G_2 of the amplifiers 1 and 2 are set so that $G_1 \geq G_{0,1}$ and $G_2 \leq G_{0,2}$. In this case, as will be described later with reference to Fig. 2, the amplifiers 1 and 2 can have gain vs wavelength characteristics that can be compensated by the combination thereof. For example, the gain of the amplifier 1 at a wavelength is large, while the gain of the amplifier 2 at the same wavelength as described above is small. Hence, the total gain obtained by the amplifiers 1 and 2 can be maintained at a constant (flat) level. ~~By combining the~~ two amplifiers together as described above, it is possible for the multi-wavelength light amplifier to have no waveform-dependence of the gain thereof.

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The above waveform-dependence of the gain can be maintained at a constant level irrespective of a variation in the input power by means of the feedback loop including the light splitting coupler 12, the photodiode 13, the ALC circuit 14 and the variable attenuator 11. The split light from the beam splitting c upler 12 is applied t the phot diode 13, which generates an electric signal corresp nding to th light level. The ab ve electric signal is applied

to the variabl attenuat r 11, and the amount f attenuati n caused therein is varied n the basis of the light level detected by the phot diode 13. In this manner, the light output level of the second-stage amplifier 2 can be maintained at a constant level. The variable attenuator 11 may be formed by using a Faraday rotator or the electro-optical effect of a lithium niobate ($LiNbO_3$) crystal.

The amplifiers 1 and 2 are pumped forward by the pump sources 9_1 and 9_2. Alternatively, it is possible to pump the amplifiers 1 and 2 backward. It is also possible to pump the amplifiers 1 and 2 forward and backward.

The light amplifier shown in Fig. 1 is capable of amplifying all the wavelengths to be multiplexed so that the light amplifier does not have the wavelength-dependence of the gain, which is not changed due to a variation in the power of the input light. If some wavelengths are not used or only some wavelengths are used, a filter (not shown) having a corresponding wavelength characteristic may be placed before the photodiode 4_1 (4_3) or 4_2 (4_4) of the first-stage (second-stage) amplifier 1 (2) or both thereof.

Fig. 2 is a diagram of the operation of a multi-wavelength light amplifier according to a second embodiment of the present invention. The second embodiment has the same configuration as shown in Fig. 1. According to the second embodiment of the present invention, the optical fibers 7 and 8 are erbium-doped (Er-doped) optical fibers, which are examples of rare-earth-element doped optical fibers. Normally, alumina (Al_2O_3) is added to the Er-doped optical fibers at a high concentration level. In this regard, the Er-doped optical fiber may be called a co-doped optical fiber. Th Er-doped optical fib r has a substantially lin ar gain vs wavelength characteristic in an amplifying band about 1550 nm, as sh wn in Fig. 2.

Part (a) f Fig. 2 shows a gain vs wavelength characteristic obtained in th amplifying band ab ut 1550 nm wh n the exciting rat is relatively high, and part (b) of Fig. 2 shows a gain vs wavelength characteristic obtained in the amplifying band about 1550 nm when the exciting rate is relative low. The characteristics shown in parts (a) and (b) of Fig. 2 are due to the characteristics of absorption/emission of Er ions in the Er-doped optical fiber with alumina added thereto at a high concentration level. The horizontal axes of the parts (a), (b) and (c) of Fig. 2 denote the wavelength, and the vertical axes thereof denote the gain of the Er-doped optical fiber.

As shown in part (a) of Fig. 2, in the amplifying band about 1550 nm, the fiber has a relatively high gain on the short-wavelength side, and a relatively low gain on the long-wavelength side. In other words, as the wavelength becomes shorter, the gain becomes higher. As shown in part (b) of Fig. 2, in the amplifying band about 1550 nm, the fiber has a relatively high gain on the long-wavelength side, and a relatively low gain on the short-wavelength side. In other words, as the wavelength becomes longer, the gain becomes higher.

According to the second embodiment of the present invention, the Er-doped fiber 7 of the first amplifier 1 is long enough to increase the exciting rate and obtain the characteristic shown in part (a) of Fig. 2. The Er-doped fiber 8 of the second amplifier 1 is short enough to decrease the exciting rate and obtain the characteristic shown in part (b) of Fig. 2. Generally, when the pumping of the Er-doped fiber is increased, the gain vs wavelength characteristic is changed from part (b) of Fig. 2 to part (a) through part (c).

The linear gain slope characteristic f the

first-stage amplifier 1 and that of th gain characteristic f the sec nd-stage amplifier 2 are canceled by the combination of the amplifiers 1 and 2, so that a flat gain vs wavelength characteristic (a spectrum characteristic having a constant gain) as shown in part (c) of Fig. 2 can be obtained.

It is preferable for the first-stage amplifier 1 to be a low noise figure. In this regard, the Er-doped fiber 7 of the first-stage amplifier is used at a relatively high exciting rate. In this case, the exciting efficiency is not high. The Er-doped fiber 8 is used at a relatively low exciting rate. Hence, it is possible to improve the exciting efficiency of the second-stage amplifier 1. This contributes to reducing energy consumed in the second-stage amplifier 2.

The following data has been obtained through an experiment in which the multi-wavelength light amplifier was actually produced. The light amplifier produced in the experiment was designed to amplify four wavelengths (1548 nm, 1551 nm, 1554 nm, 1557 nm). The light input level used in the experiment was selected so as to fall within the range of -25 dBm through -15 dBm. The gain and the gain tilt of the first-stage amplifier 1 were respectively set to 20 dB and 1.5 dB at a maximum power of the exciting light equal to -160 mW (980 nm). The second-stage amplifier 2 was adjusted so as to produce, for each channel, the light output equal to +7 dBm at a maximum power of the exciting light equal to -100 mW (1480 nm). In this case, the multi-wavelength light amplifier has a maximum noise figure of 5.6 dB and a maximum gain tilt of 0.2 dB.

Fig. 3 is a block diagram of a multi-wav length light amplifier according to a third embodiment of the present invention. In Fig. 3, parts that are the same as those shown in Fig. 1 are

indicated by the same r ference numbers. The light amplifier shown in Fig. 3 has an ptical filter 15 f r compensating for a wavelength characteristic, as will be described below. The optical filter 15 is provided between the variable attenuator 11 and the input side of the second-stage amplifier 2.

Fig. 4 is a diagram showing the operation of the light amplifier shown in Fig. 3. More particularly, part (a) of Fig. 4 shows a gain vs wavelength characteristic of the first-stage amplifier 1 shown in Fig. 3; and part (b) thereof shows a gain vs wavelength characteristic obtained by the combination of the first-stage amplifier 1 and the optical filter 15. Part (c) of Fig. 4 shows a gain vs wavelength characteristic of the second-stage amplifier 2 shown in Fig. 4, and part (d) shows a total gain vs wavelength characteristic of the whole light amplifier shown in Fig. 3.

The configuration of the first-stage amplifier 1 shown in Fig. 3 is the same as that of the amplifier 1 shown in Fig. 1. The configuration of the second-stage amplifier 2 shown in Fig. 3 is the same as that of the amplifier 2 shown in Fig. 1.

The optical filter 15 emphasizes the gain vs wavelength characteristic of the first-stage amplifier 1. As shown in parts (a) and (b) of Fig. 4, the gain for the short wavelengths is particularly emphasized. In other words, the linear gain slope of the characteristic shown in part (a) of Fig. 4 is increased by the optical filter 15. The characteristic of the second-stage amplifier 2 shown in part (c) of Fig. 4 compensates for the characteristic shown in part (b) thereof, so that the flat gain characteristic shown in part (d) of Fig. 4 can be finally obtained.

It will be n ted that the exciting rate necessary t btain the characteristic shown in part

(c) f Fig. 4 is lower than that necessary t obtain the characteristic shown in part (b) of Fig. 2. In other words, the exciting efficiency of the characteristic shown in part (c) of Fig. 4 is higher than that of the characteristic shown in part (b) of Fig. 2. Hence, the second-stage amplifier 2 shown in Fig. 3 consumes a smaller amount of energy than that shown in Fig. 1. In other words, if the second-stage amplifier 2 shown in Fig. 3 consumes the same amount of energy as that shown in Fig. 1, the multi-wavelength light amplifier shown in Fig. 3 can output a larger amount of power than that shown in Fig. 1.

Since the first-stage amplifier 1 has the characteristic shown in part (a) of Fig. 4, it is a low noise figure. The characteristic of the first-stage amplifier 1 is emphasized by the optical filter 15, and the exciting efficiency thereof may be improved.

The variable attenuator 11 shown in Fig. 3 is controlled in the same manner as that shown in Fig. 1 as has been described previously. In short, the variable attenuator 11 maintains the level of the output light of the second-stage amplifier 1 at the predetermined constant level.

Fig. 5 is a block diagram of a multi-wavelength light amplifier according to a fourth embodiment of the present invention. In Fig. 5, parts that are the same as those shown in the previously described figures are given the same reference numbers. The configuration shown in Fig. 5 differs from that shown in Fig. 3 in that the optical filter 15 shown in Fig. 5 is provided between the output side of the second-stage amplifier 2 and the beam splitting coupler 12.

Fig. 6 is a diagram showing the operation of the light amplifier shown in Fig. 5. Mor particularly, part (a) of Fig. 6 shows a gain vs

wavelength characteristic of the first-stage amplifier 1 sh wn in Fig. 5, and part (b) there f shows a gain vs wavelength characteristic of the second-stage amplifier 2 shown in Fig. 5. Part (c) of Fig. 5 is a gain vs wavelength characteristic obtained by the combination of the first-stage amplifier 1 and the second-stage amplifier 2. Part (d) of Fig. 6 shows a total gain vs wavelength characteristic of the whole light amplifier shown in Fig. 5.

The configuration of the first-stage amplifier 1 shown in Fig. 5 is the same as that of the amplifier 1 shown in Figs. 1 and 3. The configuration of the second-stage amplifier 2 shown in Fig. 5 is the same as that of the amplifier 2 shown in Figs. 1 and 3.

The optical filter 15 has a gain vs wavelength characteristic which compensates for that shown in part (b) of Fig. 2. As shown in parts (a) and (b) of Fig. 6, the characteristic of the second-stage amplifier 2 is pumped so as to have an emphasized gain vs wavelength characteristic, as compared to that of the first-stage amplifier 1. In the emphasized characteristic, the gain for the long wavelengths is particularly emphasized. In other words, the linear gain slope of the characteristic shown in part (b) of Fig. 6 is greater than that shown in part (a) thereof although the linear gain slopes shown in parts (a) and (b) thereof are oriented in different directions. The combination of the first-stage amplifier 1 and the second-stage amplifier 2 results in the characteristic shown in part (c) of Fig. 6. It is not required that the first-stage amplifier 1 and the second-stage amplifier 2 have characteristics of such a difference which can be completely canceled by the combination thereof.

The optical filter 15 sh wn in Fig. 5 has a gain vs wavelength characteristic which compensates

for the charact ristic sh wn in part (c) of Fig. 6. Thus, the t tal characteristic is as sh wn in part (d) of Fig. 6.

It will be noted that the exciting rate necessary to obtain the characteristic shown in part (b) of Fig. 6 is lower than that necessary to obtain the characteristic shown in part (b) of Fig. 2. In other words, the exciting efficiency of the characteristic shown in part (b) of Fig. 6 is higher than that of the characteristic shown in part (b) of Fig. 2. Hence, the second-stage amplifier 2 shown in Fig. 5 consumes a smaller amount of energy than that shown in Fig. 1. In other words, if the second-stage amplifier 2 shown in Fig. 5 consumes the same amount of energy as that shown in Fig. 1, the multi-wavelength light amplifier shown in Fig. 5 can output a larger amount of power than that shown in Fig. 1.

The variable attenuator 11 shown in Fig. 5 is controlled in the same manner as that shown in Fig. 1 as has been described previously. In short, the variable attenuator 11 shown in Fig. 5 maintains the level of the output light of the second-stage amplifier 1 at the predetermined constant level.

The optical filter 15 used in Fig. 3 or Fig. 5 may be a conventional coupler of a melting attachment type. By adjusting the wavelength period of the coupler, it is possible to use the coupler as a gain tilting filter. For example, the optical filter 15 shown in Fig. 5 has a gain tilt equal to approximately 3 dB in order to obtain the flat gain characteristic shown in part (d) of Fig. 6.

A description will now be given of a multi-wavelength light amplifier according to a fifth embodiment of the present invention. This embodiment is intended to obtain the same functi n as the c nfiguration shown in Fig. 3 without the ptical filter 15 shown therein. In other words, the light

amplifi r ac rding to th fifth emb diment is configur d as shown in Fig. 1, nevertheless it has the function of the light amplifier shown in Fig. 3.

According to the fifth embodiment of the present invention, the beam splitting coupler 5_2 is replaced by a beam splitting coupler 21 shown in Fig. 7A, which has a transparent rate vs wavelength characteristic as shown in Fig. 7B. In Fig. 7A, a pump source 22 which corresponds to the pump source 9_2 is coupled to the beam splitting coupler 21. In Fig. 7B, symbol λ_p denotes the wavelength of the pump light emitted from the source 22. Symbol λ_s denotes the central wavelength of the multiplexed light signal. Symbols λ_{s1} and λ_{sn} are wavelengths which define the band of the multiplexed light signal. A solid line shown in Fig. 7B denotes a characteristic used for communications. Two dot lines are obtained by shifting the solid line. As indicated by the solid line, the beam splitting coupler 21 functions to pass the multiplexed signal light and prevent the pump light in the forward direction.

By shifting the solid line toward the short-wavelength side as indicated by character A in Fig. 7B, the characteristic curve of the transparent rate has a slope in the band defined by the wavelengths λ_{s1} and λ_{sn}. In this case, the highest transparent rate can be obtained at the shortest wavelength λ_{s1}, and the lowest transparent rate can be obtained at the longest wavelength λ_{sn}. This characteristic corresponds to the characteristic of the optical filter 15 used in the configuration shown in Fig. 3. With the above configuration, the multi-wavelength light amplifier according to the fifth embodiment of the present invention has the same advantages as those of the light amplifier sh wn in Fig. 3.

The beam splitting coupler 21 can b applied t the first-stage amplifier 1 instead of the second-

stage amplifier 2. In this cas , the Er-doped optical fiber 7 f the first-stag amplifier 1 is pumped backward by the pump source 22 because the optical filter 15 shown in Fig. 3 is placed on the output side of the Er-doped optical fiber 7.

A description will now be given of a multi-wavelength light amplifier according to a sixth embodiment of the present invention. This embodiment is intended to obtain the same function as the configuration shown in Fig. 5 without the optical filter 15 shown therein. In other words, the light amplifier according to the sixth embodiment is configured as shown in Fig. 1, nevertheless it has the function of the light amplifier shown in Fig. 5.

In the sixth embodiment of the present invention, the pump source 9_2 shown in Fig. 1 is replaced by the pump source 22 shown in Fig. 7A having the transparent rate characteristic indicated by B shown in Fig. 7B in such a way that the Er-doped optical fiber 8 is pumped backward by the pump source 22. This is because the optical filter 15 shown in Fig. 5 is placed on the output side of the Er-doped optical fiber 8 shown in Fig. 5.

By shifting the solid line shown in Fig. 7B toward the long-wavelength side as indicated by character B, the characteristic curve of the transparent rate has a slope in the band defined by the wavelengths λ_{s1} and λ_{sn}. In this case, the highest transparent rate can be obtained at the longest wavelength λ_{sn}, and the lowest transparent rate can be obtained at the shortest wavelength λ_{s1}. This characteristic corresponds to the characteristic of the optical filter 15 used in the configuration shown in Fig. 5. With the above configuration, the multi-wavelength light amplifier acc rding t the sixth embodiment f th present inventi n has the same advantages as those of th light amplifier shown in

Fig. 5.

It will be not d that th above-mentioned third through sixth embodiments of the present invention may be combined appropriately.

Fig. 8 is a multi-wavelength light amplifier according to a seventh embodiment of the present invention. In Fig. 8, parts that are the same as those shown in the previously described figures are given the same reference numbers. The light amplifier shown in Fig. 8 has a second-stage light amplifier 2A having a configuration different from the above-mentioned second-stage light amplifier 2.

More particularly, the second-stage amplifier 2A has an automatic power control (APC) circuit 10. The APC circuit 10 monitors and controls the pump light emitted from the pump source 9_2, so that the pump light can be emitted at a predetermined constant level. As has been described previously, the variable attenuator 11 functions to maintain the amplified light output by the second-stage amplifier 2 at the predetermined constant level. Hence, even by the automatic power control of the pump light directed to maintaining the pump light at the constant level, it is possible to maintain the output light of the second-stage amplifier 2A at the predetermined constant level even if the power of the light input signal fluctuates.

The first-stage amplifier 1 shown in Fig. 8 has a gain vs wavelength characteristic as shown in part (a) of Fig. 2, and the second-stage amplifier 2A shown in Fig. 8 has a gain vs wavelength characteristic as shown in part (b) of Fig. 2.

The second-stage amplifier 2A does not need the c uplers 3_3 and 3_4, and th phot di des 4_3 and 4_4. H nc , the second-stag amplifier 2A is simpler than the sec nd-stage amplifier 2, so that down-sizing of the light amplifier can be facilitat d.

Fig. 9 is a block diagram of a multi-wavelength light amplifier according to an ighth embodiment of the present inventi n. In Fig. 9, parts that are the same as those shown in the previously described figures are given the same reference numbers. The configuration shown in Fig. 9 differs from the configuration shown in Fig. 1 in that the variable attenuator 11 shown in Fig. 9 is provided n the output side of the second-stage amplifier 2. Thus, the variable attenuator 11 attenuates the output light signal of the second-stage amplifier 2 so that it can be maintained at the predetermined constant level.

It will be noted that in the configuration shown in Fig. 1, the attenuated light signal from the variable attenuator 11 is amplified by the second-stage amplifier 2. On the other hand, in the configuration shown in Fig. 9, the variable attenuat r 11 attenuates the light output signal of the second-stage amplifier 2. Hence, the second-stage amplifier 2 shown in Fig. 9 needs a much larger amount of energy of the pump light than that used in the configuration shown in Fig. 1. However, except for the above, the light amplifier shown in Fig. 9 has the same advantages as the configuration shown in Fig. 1. For example, the light amplifier shown in Fig. 9 has a low noise figure because an increase in loss of the gain does not occur between the first-stage amplifier 1 and the second-stage amplifier 2.

It will be noted that the first-stage and second-stage amplifiers 1 and 2 (2A) are not limited to the previously described AGC (APC) circuits in order to obtain the characteristics shown in Figs. 2, 4 and 6. It is possible to arbitrarily combine the previously described AGC circuits. Further, it is also possible to employ ther AGC circuits or quivalents there f, which will be described bel w as

ninth thr ugh lev nth emb diments of th present inventi n. It will be noted that the AGC circuit f the first-stage circuit can be selected separately from the AGC circuit of the second-stage circuit.

Fig. 10 is a block diagram of a multi-wavelength light amplifier according to a ninth embodiment of the present invention, wherein parts that are the same as those shown in Fig. 1 are given the same reference numbers. The light amplifier shown in Fig. 10 has a first-stage amplifier 1B and a second-stage amplifier 2B, which are different from the amplifiers 1 and 2.

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The first-stage amplifier 1B, which has a gain vs wavelength characteristic as shown in part (a) of Fig. 2, has a forward-direction photodiode 20_1, which detects an amplified spontaneous emission (ASE) leaking from the side surface of the Er-doped optical fiber 7. The AGC circuit 6_1 is supplied with the output signal of the photodiode 20_1 and controls the pump power of the pump source 9_1 so that the amplified spontaneous emission can be maintained at a predetermined constant level. As a result of the AGC control, the gain of the front-stage amplifier 1B can be maintained at the predetermined constant value.

Similarly, the second-stage amplifier 2B, which has a gain vs wavelength characteristic as shown in part (b) of Fig. 2, has a forward-direction photodiode 20_2, which detects the amplified spontaneous emission leaking from a side surface of the Er-doped optical fiber 8. The AGC circuit 6_2 is supplied with the output signal of the photodiode 20_2 and controls the pump power of the pump source 9_2 so that the amplified spontaneous emission can be maintained at a predetermined constant level. As a result of the abov AGC contr l, the gain of th second-stage amplifier 2B can b maintained at the predetermined constant level.

As has been described previ usly, the variable attenuator 11 provid d betw en the first-stage amplifier 1B and the second-stage amplifier 2B functions to maintain the light output level at the predetermined constant level.

Fig. 11 is a block diagram of a multi-wavelength light amplifier according to a tenth embodiment of the present invention, in which parts that are the same as those shown in the previously described figures are given the same reference numbers. The light amplifier shown in Fig. 11 includes a first-stage light amplifier 1C and a second-stage light amplifier 2C.

The first-stage light amplifier 1C, which has a gain vs wavelength characteristic as shown in part (a) of Fig. 2, includes a WDM coupler 16_1 and a photodiode 17_1. The WDM coupler 16_1 separates the light in the 1530 nm band (ASE) from the light in the 1550 nm band (signal light). The above ASE travels toward the input side of the Er-doped optical fiber 7 (backward ASE). The photodiode 17_1 detects the amplified spontaneous emission of the Er-doped optical fiber 7. The AGC circuit 6_1 receives the output signal of the photodiode 17_1 and controls the pump power of the pump source 9_1 so that the backward ASE can be maintained at a predetermined constant level. As a result of the above AGC control, the gain of the first-stage amplifier 1C can be maintained at the predetermined constant level.

The second-stage light amplifier 2C, which has a gain vs wavelength characteristic as shown in part (b) of Fig. 2, includes a WDM coupler 16_2 and a photodiode 17_2. The WDM coupler 16_1 separates the light in the 1530 nm band (ASE) from th light in the 1550 nm band (signal light). The abov ASE travels toward the input sida of the Er-doped optical fiber 8 (backward ASE). The ph t diod 17_2 detects the

amplified sp ntaneous emissi n of the Er-d ped ptical fiber 8. The AGC circuit 6_2 receives the utput signal of the photodiode 17_2 and c ntrols the pump power of the pump source 9_2 so that the backward ASE can be maintained at a predetermined constant level. As a result of the above AGC control, the gain of the second-stage amplifier 2C can be maintained at the predetermined constant level.

As has been described previously, the variable attenuator 11 provided between the first-stage amplifier 1C and the second-stage amplifier 2C functions to maintain the light output level at the predetermined constant level.

Fig. 12 is a block diagram of a multi-wavelength light amplifier according to an eleventh embodiment of the present invention, in which parts that are the same as those shown in the previously described figures are given the same reference numbers. The light amplifier shown in Fig. 12 includes a first-stage light amplifier 1D and a second-stage light amplifier 2D.

The first-stage light amplifier 1D, which has a gain vs wavelength characteristic as shown in part (a) of Fig. 2, includes a WDM coupler 5_3 and a photodiode 18_1. The WDM coupler 5_3 is provided on the output side of the Er-doped optical fiber 7, and separates the residual pump light (exciting light) propagated through the fiber 7 from the signal light. The residual pump light separated by the WDM coupler 5_3 is applied to the photodiode 18_1, which outputs a corresponding electric signal to the AGC circuit 6_1. Then, the AGC circuit 6_1 controls the pump power of the pump source 9_1 on the basis of the detected residual pump light so that the residual pump light can be maintained at a predet rmined constant level. As a result f the ab ve AGC control, the gain of the first-stage amplifier 1D can be maintained at the

predetermined constant level.

The second-stage light amplifier 2D, which has a gain vs wavelength characteristic as shown in part (b) of Fig. 2, includes a WDM coupler 5_4 and a photodiode 18_2. The WDM coupler 5_4 is provided on the output side of the Er-doped optical fiber 8, and separates the residual pump light (exciting light) propagated through the fiber 8 from the signal light. The residual pump light separated by the WDM coupler 5_4 is applied to the photodiode 18_2, which outputs a corresponding electric signal to the AGC circuit 6_2. Then, the AGC circuit 6_2 controls the pump power of the pump source 9_2 on the basis of the detected residual pump light so that the residual pump light can be maintained at a predetermined constant level. As a result of the above AGC control, the gain of the second-stage amplifier 2D can be maintained at the predetermined constant level.

As has been described previously, the variable attenuator 11 provided between the first-stage amplifier 1D and the second-stage amplifier 2D functions to maintain the light output level at the predetermined constant level.

Fig. 13 is a block diagram of a multi-wavelength light amplifier according to a twelfth embodiment of the present invention, wherein parts that are the same as those shown in the previously described figures are given the same reference numbers. The light amplifier shown in Fig. 13 differs from that shown in Fig. 1 in that the beam splitting coupler 12 is provided between the variable attenuator 11 and the second-stage amplifier 2.

It is possible to maintain the light output of the second-stage amplifier 2 at the predetermined constant level by controlling the variabl attenuator 11 on the basis of the attenuat d light output so that the attenuated light output is maintained at a

predetermined constant level. In rder to realize the ab ve feedback contr l, the ph todiode 13 detects a split component of the attenuat d light output, and the ALC circuit 14 controls the variable attenuator 11 in the above-described manner.

Fig. 14 is a block diagram of a multi-wavelength light amplifier according to a thirteenth embodiment of the present invention, in which parts that are the same as those shown in the previously described figures are given the same reference numbers. The light amplifier shown in Fig. 14 corresponds to a modification of the light amplifier shown in Fig. 13. The light amplifier shown in Fig. 14 has the first-stage light amplifier 1 and a second-stage light amplifier 2E.

The second-stage light amplifier 2E, which has a gain vs wavelength characteristic as shown in part (b) of Fig. 2, includes a beam splitting coupler 3_4, the photodiode 4_4 and an ALC circuit 14_2. It will be noted that the second-stage amplifier 2E is simpler than the second-stage amplifier 2 shown in Fig. 13. As has been described previously with reference to Fig. 13, the attenuated light output is maintained at the predetermined constant level. Hence, the operation of the second-stage amplifier 2E receiving the attenuated light output through the beam splitting coupler 12 is equivalent to the AGC-controlled operation of the second-stage amplifier. Hence, it is possible to control the pump power of the pump source 9_2 by the automatic level control performed by the ALC circuit 14_2.

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Fig. 15 shows a multi-wavelength light amplifier according to a fourteenth embodiment of the present invention. This amplifier includes a r j cti n filter 30 provided between the first-stage amplifier 1 and the second-stage amplifier 2. The rejecti n filter 30 prevents the pump light propagated

fr m th Er-d ped ptical fiber 7 fr m passing therethrough, and impr ves the exciting efficiency f the second-stage amplifier 2. The rejection filter 30 can be applied to the other embodiments of the present invention in the same manner as shown in Fig. 15.

The above-described embodiments of the present invention can be arbitrarily combined to provide variations and modifications.

The present invention is not limited to the specifically disclosed embodiments, and variations and modifications may be made without departing from the scope of the present invention.